MB39C603

MB39C603 is a Primary Side Regulation (PSR) LED driver IC for LED lighting. Using the information of the primary peak current and the transformer-energy-zero time, it is able to deliver a well regulated current to the secondary side without using an opto-coupler in an isolated flyback topology. Operating in critical conduction mode, a smaller transformer is required. In addition, MB39C603 has a built-in phase dimmable circuit and can constitute flicker less lighting systems for phase dimming with low-component count. It is most suitable for the general lighting applications, for example replacement of commercial and residential incandescent lamps.
Features
■PSR topology in an isolated flyback circuit
■High power factor (>0.9 : without dimmer) in Single Conversion
■High efficiency (>80\% : without dimmer) and low EMI by detecting transformer zero energy
■ Built-in phase dimmable circuit

- Dimming curve based on conduction angle
- Dimmer hold current control
- Highly reliable protection functions
- Under voltage lock out (UVLO)
$\square$ Over voltage protection (OVP)
$\square$ Over current protection (OCP)
- Over temperature protection (OTP)
■Switching frequency setting : 30 kHz to 133 kHz
■ Input voltage range VDD : 9V to 20V
■ Input voltage for LED lighting applications : AC110V ${ }_{\text {RMS }}$
■Output power range for LED lighting applications: 15W to 50W
■Package : SOP-14 (5.30 mm $\times 10.15 \mathrm{~mm} \times 2.25 \mathrm{~mm}[\mathrm{Max}]$ )
Applications
■ Phase dimmable (Leading/Trailing) LED lighting
■LED lighting


## Contents

1. Pin Assignment ..... 3
2. Pin Descriptions ..... 3
3. Block Diagram ..... 4
4. Absolute Maximum Ratings ..... 5
5. Recommended Operating Conditions ..... 6
6. Electrical Characteristics ..... 7
7. Standard Characteristics ..... 9
8. Function Explanations ..... 10
8.1 LED Current Control by PSR(Primary Side Regulation) ..... 10
8.2 PFC (Power Factor Correction) Function ..... 11
8.3 Phase Dimming Function ..... 11
8.4 HOLD Current Control Function ..... 12
8.5 Power-On Sequence ..... 13
8.6 Power-Off Sequence ..... 14
8.7 Ip_peak Detection Function ..... 14
8.8 Zero Voltage Switching Function ..... 14
8.9 Protection Functions ..... 15
9. I/O Pin Equivalent Circuit Diagram ..... 16
10. Application Examples. ..... 18
10.1 17W Isolated and Phase Dimming Application ..... 18
11. Usage Precautions. ..... 26
12. Ordering Information ..... 27
13. Marking Format ..... 27
14. Recommended Mounting Condition [JEDEC Level3] Lead Free ..... 28
14.1 Recommended Reflow Condition ..... 28
14.2 Reflow Profile ..... 28
15. Package Dimensions ..... 29
16. Major Changes ..... 30
Document History ..... 31

## 1. Pin Assignment

Figure 1-1 Pin Assignment


## 2. Pin Descriptions

Table 2-1 Pin Descriptions

| Pin No. | Pin Name | I/O | Description |
| :---: | :---: | :---: | :--- |
| 1 | NC | - | Not used. Leave this pin open. |
| 2 | VDD | - | Power supply pin. |
| 3 | TZE | I | Transformer Zero Energy detecting pin. |
| 4 | COMP | O | External Capacitor connection pin for the compensation. |
| 5 | HOLDDET | I | Phase Dimmer current detecting pin. |
| 6 | HOLDCNT | O | External BIP base current control pin. |
| 7 | NC | - | Not used. Leave this pin open. |
| 8 | NC | - | Not used. Leave this pin open. |
| 9 | VAC | I | Phase Dimmer conduction angle detecting pin. |
| 10 | ADJ | O | Pin for adjusting the switch-on timing. |
| 11 | CS | I | Pin for detecting peak current of transformer primary winding. |
| 12 | GND | - | Ground pin. |
| 13 | DRV | O | External MOSFET gate connection pin. |
| 14 | NC | - | Not used. Leave this pin open. |

## 3. Block Diagram

Figure 3-1 Block Diagram (Isolated Flyback Application)


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## 4. Absolute Maximum Ratings

Table 4-1 Absolute Maximum Ratings

| Parameter | Symbol | Condition | Rating |  | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min | Max |  |
| Power Supply Voltage | $\mathrm{V}_{\mathrm{VDD}}$ | VDD pin | -0.3 | +25 | V |
| Input Voltage | $\mathrm{V}_{\text {cs }}$ | CS pin | -0.3 | +6.0 | V |
|  | $V_{\text {TZE }}$ | TZE pin | -0.3 | +6.0 | V |
|  | $\mathrm{V}_{\text {Holddet }}$ | HOLDDET pin | -0.3 | +6.0 | V |
|  | V VAC | VAC pin | -0.3 | +6.0 | V |
| Output Voltage | $V_{\text {DRV }}$ | DRV pin | -0.3 | +25 | V |
|  | $\mathrm{V}_{\text {Holdcnt }}$ | HOLDCNT pin | -0.3 | +6.0 | V |
| Output Current | $\mathrm{I}_{\text {ADJ }}$ | ADJ pin | -1 | - | mA |
|  | IDRV | DRV pin DC level | -50 | +50 | mA |
|  | Iholdent | HOLDCNT pin | -400 | - | $\mu \mathrm{A}$ |
| Power Dissipation | $\mathrm{P}_{\mathrm{D}}$ | $\mathrm{Ta} \leq+25^{\circ} \mathrm{C}$ | - | 500(*1) | mW |
| Storage Temperature | TSTG | - | -55 | +125 | ${ }^{\circ} \mathrm{C}$ |
| ESD Voltage 1 | $\mathrm{V}_{\text {ESDH }}$ | Human Body Model | -2000 | +2000 | V |
| ESD Voltage 2 | $V_{\text {ESDC }}$ | Charged Device Model | -1000 | +1000 | V |

*1: The value when using two layers PCB.
Reference: $\theta \mathrm{ja}$ (wind speed $0 \mathrm{~m} / \mathrm{s}$ ): $200^{\circ} \mathrm{C} / \mathrm{W}$

Figure 4-1 Power Dissipation


## WARNING:

1. Semiconductor devices may be permanently damaged by application of stress (including, without limitation, voltage, current or temperature) in excess of absolute maximum ratings. Do not exceed any of these ratings.

MB39C603

## 5. Recommended Operating Conditions

Table 5-1 Recommended Operating Conditions

| Parameter | Symbol | Condition | Value |  |  | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min | Typ | Max |  |
| VDD pin Input Voltage | V VDD | VDD pin | 9 | - | 20 | V |
| VAC pin Resistance | Rvac | VAC pin | - | 510 | - | $\mathrm{k} \Omega$ |
| TZE pin Resistance | $\mathrm{R}_{\text {TZE }}$ | TZE pin | 50 | - | 200 | $\mathrm{k} \Omega$ |
| ADJ pin Resistance | $\mathrm{R}_{\text {ADJ }}$ | ADJ pin | 9.3 | - | 185.5 | $\mathrm{k} \Omega$ |
| COMP pin Capacitance | $\mathrm{C}_{\text {comp }}$ | COMP pin | - | 4.7 | - | $\mu \mathrm{F}$ |
| VDD pin Capacitance | $\mathrm{C}_{\text {BP }}$ | Set between VDD pin and GND pin | - | 100 | - | $\mu \mathrm{F}$ |
| Operating Junction Temperature | Tj | - | -40 | - | +125 | ${ }^{\circ} \mathrm{C}$ |

## WARNING:

1. The recommended operating conditions are required in order to ensure the normal operation of the semiconductor device. All of the device's electrical characteristics are warranted when the device is operated under these conditions.
2. Any use of semiconductor devices will be under their recommended operating condition.
3. Operation under any conditions other than these conditions may adversely affect reliability of device and could result in device failure.
4. No warranty is made with respect to any use, operating conditions or combinations not represented on this data sheet. If you are considering application under any conditions other than listed herein, please contact sales representatives beforehand.

## 6. Electrical Characteristics

Table 6-1 Electrical Characteristics

| $\left(\mathrm{Ta}=+25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{VDD}}=12 \mathrm{~V}\right)$ |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Parameter |  | Symbol | Pin | Condition | Value |  |  | Unit |
|  |  | Min |  |  | Typ | Max |  |
| UVLO | UVLO Turn-on threshold voltage |  | $\mathrm{V}_{\text {TH }}$ | VDD | - | 9.6 | 10.2 | 10.8 | V |
|  | UVLO Turn-off threshold voltage | $\mathrm{V}_{\text {TL }}$ | VDD | - | 7.55 | 8 | 8.5 | V |
|  | Startup current | $I_{\text {Start }}$ | VDD | $\mathrm{V}_{\mathrm{VDD}}=7 \mathrm{~V}$ | - | 65 | 160 | $\mu \mathrm{A}$ |
| TRANSFORMER ZERO ENERGY DETECTION | Zero energy threshold voltage | $\mathrm{V}_{\text {TZETL }}$ | TZE | TZE = "H" to "L" | - | 20 | - | mV |
|  | Zero energy threshold voltage | $\mathrm{V}_{\text {TZETH }}$ | TZE | TZE = "L" to "H" | 0.6 | 0.7 | 0.8 | V |
|  | TZE clamp voltage | $\mathrm{V}_{\text {TZECLAMP }}$ | TZE | $\mathrm{I}_{\text {TZE }}=-10 \mu \mathrm{~A}$ | -200 | -160 | -100 | mV |
|  | OVP threshold voltage | $\mathrm{V}_{\text {TZEOVP }}$ | TZE | - | 4.15 | 4.3 | 4.45 | V |
|  | OVP blanking time | tovpblank | TZE | - | 0.6 | 1 | 1.7 | $\mu \mathrm{s}$ |
|  | TZE input current | $I_{\text {TZE }}$ | TZE | $\mathrm{V}_{\text {TZE }}=5 \mathrm{~V}$ | -1 | - | +1 | $\mu \mathrm{A}$ |
| COMPENSATION | Source current | Iso | $\underset{\mathrm{P}}{\mathrm{COM}}$ | $\mathrm{V}_{\text {COMP }}=2 \mathrm{~V}, \mathrm{~V}_{\mathrm{CS}}=0 \mathrm{~V}$, Conduction Angle = 165deg | - | -27 | - | $\mu \mathrm{A}$ |
|  | Trans conductance | gm | $\begin{gathered} \text { COM } \\ \mathrm{P} \end{gathered}$ | $\mathrm{V}_{\text {COMP }}=2.5 \mathrm{~V}, \mathrm{~V}_{\text {CS }}=1 \mathrm{~V}$ | - | 96 | - | $\mu \mathrm{V} /$ |
| ADJUSTMENT | ADJ voltage | $\mathrm{V}_{\text {ADJ }}$ | ADJ | - | 1.81 | 1.85 | 1.89 | V |
|  | ADJ source current | $\mathrm{I}_{\text {ADJ }}$ | ADJ | $\mathrm{V}_{\mathrm{ADJ}}=0 \mathrm{~V}$ | -650 | -450 | -250 | $\mu \mathrm{A}$ |
|  | ADJ time | $t_{\text {ADJ }}$ | $\begin{aligned} & \text { TZE } \\ & \text { DRV } \end{aligned}$ | $\begin{aligned} & \mathrm{t}_{\mathrm{ADJ}}\left(\mathrm{R}_{\mathrm{ADJ}}=51 \mathrm{k} \Omega\right)- \\ & \mathrm{t}_{\mathrm{ADJ}}\left(R_{\mathrm{ADJ}}=9.1 \mathrm{k} \Omega\right) \end{aligned}$ | 490 | 550 | 610 | ns |
|  | Minimum switching period | Tsw | $\begin{aligned} & \text { TZE } \\ & \text { DRV } \end{aligned}$ | - | 6.75 | 7.5 | 8.25 | $\mu \mathrm{s}$ |
| CURRENT SENSE | OCP threshold voltage | $\mathrm{V}_{\text {OCPTH }}$ | CS | - | 1.9 | 2 | 2.1 | V |
|  | OCP delay time | tocpdiy | CS | - | - | 400 | 500 | ns |
|  | CS input current | Ics | CS | $\mathrm{V}_{\mathrm{CS}}=5 \mathrm{~V}$ | -1 | - | +1 | $\mu \mathrm{A}$ |



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## 7. Standard Characteristics

Figure 7-1 Standard Characteristics


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## 8. Function Explanations

### 8.1 LED Current Control by PSR(Primary Side Regulation)

MB39C603 regulates the average LED current (lLed) by feeding back the information based on Primary Winding peak current ( $I_{\text {P_PEAK }}$ ), Secondary Winding energy discharge time ( $\mathrm{T}_{\mathrm{DIS}}$ ) and switching period ( $\mathrm{T}_{\text {Sw }}$ ). Figure 8-1 shows the operating waveform in steady state. IP is Primary Winding current and $I_{S}$ is Secondary Winding current. ILED as an average current of the Secondary Winding is described by the following equation.

$$
I_{L E D}=\frac{1}{2} \times I_{S_{-} P E A K} \times \frac{T_{D I S}}{T_{S W}}
$$

Using $I_{\text {P_PEAK }}$ and the transformer Secondary to Primary turns ratio $\left(N_{P} / N_{S}\right)$, Secondary Winding peak current ( $I_{S_{\text {_PEAK }}}$ ) is described by the following equation.

$$
I_{S_{-} P E A K}=\frac{N_{P}}{N_{S}} \times I_{P_{-} P E A K}
$$

Therefore,

$$
I_{L E D}=\frac{1}{2} \times \frac{N_{P}}{N_{S}} \times I_{P_{-} P E A K} \times \frac{T_{D I S}}{T_{S W}}
$$

MB39C603 detects $T_{\text {DIS }}$ by monitoring the TZE pin and $I_{\text {P_PEAK }}$ by monitoring the CS pin and then controls $I_{\text {Led. }}$. An internal Err Amp sinks gm current proportional to $I_{\text {P_PEAK }}$ from the COMP pin during $T_{\text {DIS }}$ period. In steady state, since the average of the gm current is equal to internal reference current ( $\mathrm{I}_{\mathrm{so}}$ ), the voltage on the COMP pin ( $\mathrm{V}_{\text {comp }}$ ) is nearly constant.

$$
I_{P_{-} P E A K} \times R_{C S} \times g m \times T_{D I S}=I_{S O} \times T_{S W}
$$

In above equation, gm is transconductance of the Err Amp and $\mathrm{R}_{\mathrm{Cs}}$ is a sense resistance.
Eventually, ILED can be calculated by the following equation.

$$
I_{L E D}=\frac{1}{2} \times \frac{N_{P}}{N_{S}} \times \frac{I_{S O}}{g m} \times \frac{1}{R_{C S}}
$$

Figure 8-1 LED Current Control Waveform


MB39C603

### 8.2 PFC (Power Factor Correction) Function

Switching on time ( $\mathrm{T}_{\mathrm{ON}}$ ) is generated by comparing $\mathrm{V}_{\text {Сомр }}$ with an internal sawtooth waveform (refer to Figure $3-1$ ). Since $\mathrm{V}_{\text {Comp }}$ is slow varying with connecting an external capacitor ( $\mathrm{C}_{\text {COMP }}$ ) from the COMP pin to the GND pin, $\mathrm{T}_{\text {ON }}$ is nearly constant within an AC line cycle. In this state, $I_{\text {P_PEAK }}$ is nearly proportional to the AC line voltage ( $\mathrm{V}_{\text {BULK }}$ ). It can bring the phase differences between the input voltage and the input current close to zero, so that high Power Factor can be achieved.

### 8.3 Phase Dimming Function

MB39C603 is compatible with both leading-edge dimmers (TRIAC dimming) and trailing-edge dimmers
To realize the phase dimming, this device has two functions, dimmer conduction angle detect function for LED current control and TRIAC dimmer hold current control function.

Figure 8-2 shows how MB39C603 detects the conduction angle. V Bulk $^{\text {is scaled via a resistor divider connected to the VAC pin. }}$ The conduction angle is detected by monitoring the voltage on the VAC pin ( $\mathrm{V}_{\mathrm{vac}}$ ).

MB39C603 measures a half of power cycle period (Tpow) as duration between negative crossings of $\mathrm{V}_{\text {vac }}$ and a Phase Comp threshold voltage ( $\mathrm{V}_{\text {PHTH2 }}$ ). Dimmer-ON period (Tdim) is measured as duration between a positive crossing of $\mathrm{V}_{\mathrm{VAC}}$ and another Phase Comp threshold voltage ( $\mathrm{V}_{\text {PHTH1 }}$ ) and the following negative crossing. Conduction angle is defined as Tdim/Tpow $\times 180^{\circ}$.

Figure 8-2 Conduction Angle Detection Waveform


MB39C603 regulates LED current by changing a reference of Err Amp as a function of the conduction angle. Table 8-1 shows ILED dimming ratio based on the conduction angle.

In addition, the initial $\mathrm{I}_{\text {LED }}$ ratio in Power-On state is 5\%.

Table 8-1 Led Ratio Based on Conduction Angles

| Conduction Angle | $\quad$ LLED Ratio [\%] |
| :--- | :--- |
| $\theta<45 \mathrm{deg}$ | 5 |
| $45 \mathrm{deg} \leq \theta<90 \mathrm{deg}$ | $(25 / 45) \times \theta-20$ |
| $90 \mathrm{deg} \leq \theta<135 \mathrm{deg}$ | $(70 / 45) \times \theta-110$ |
| $135 \mathrm{deg} \leq \theta$ | 100 |

MB39C603

### 8.4 HOLD Current Control Function

The hold current control function prevents LEDs from flickering caused by shortage of hold current. The hold current (l $\mathrm{l}_{\text {ноLD }}$ ) is the minimum current required to flow through TRIAC dimmer in order to keep the TRIAC on (refer to Figure 8-3). In small conduction angle, since $I_{\text {LED }}$ can be low, AC/DC Converter current ( $l_{\text {BULK }}$ ) and TRIAC dimmer current ( $\mathrm{I}_{\text {TRIAC }}$ ) are reduced. Once $\mathrm{I}_{\text {TRIAC }}$ falls below $I_{\text {HoLD }}$, TRIAC goes off and this results in LED flickering. MB39C603 controls $I_{\text {TRIAC }}$ larger than $I_{\text {HoLD }}$ by adding the current ( $I_{\text {BIP }}$ ) via a BIP transistor (M1) with sensing $I_{\text {TRIAC }}$ and keeps the TRIAC on.
$I_{\text {TRIAC }}$ is sensed with a resistor ( $\mathrm{R}_{\mathrm{S}}$ ). A bypass diode ( $\mathrm{D}_{\text {BYPASS }}$ ) is used to clamp the voltage between $\mathrm{R}_{S}$ terminals ( $\mathrm{V}_{\mathrm{RS}}$ ) and prevent the voltage on the HOLDDET pin (V $V_{\text {Holddet }}$ ) from exceeding absolute maximum ratings. An offset resistor ( $\mathrm{R}_{\text {OFFSET }}$ ) is used to add an offset voltage to $\mathrm{V}_{\text {HOLDDET }}$ and prevent $\mathrm{V}_{\text {HOLDDET }}$ from the above ratings.
$R_{S}$ is set as the following equation.

$$
R_{S}=\frac{R_{\text {OFFSET }} \times I_{\text {HOLDDET }}-V_{\text {HOLDTH }}}{I_{\text {TRIACMIN }}}
$$

where $\mathrm{I}_{\text {holddet }}$ is the current of the HOLDDET pin, $\mathrm{V}_{\text {Holdth }}$ is Hold Amp threshold voltage, and $\mathrm{I}_{\text {TRIACmin }}$ is minimum TRIAC current chosen by designers.
$R_{\text {OFFSET }}$ is set as the following equation.

$$
R_{O F F S E T}>\frac{V_{B Y P A S S M A X}-0.3 \mathrm{~V}}{I_{H O L D D E T}}
$$

where $\mathrm{V}_{\text {BYPASSMAX }}$ is the maximum forward voltage of $D_{\text {BYPASS }}$.
Hold Amp is designed only for driving BIP transistors. Connecting a resistor ( $\mathrm{R}_{\text {BASE }}$ ) between the HOLDCNT pin and M1 base terminal limits the maximum IBIP value and clamp the rush current at TRIAC dimmer-on timing.

Figure 8-3 HOLD Current Control Waveform


MB39C603

### 8.5 Power-On Sequence

When the $A C$ line voltage is supplied, $\mathrm{V}_{\text {BULK }}$ is powered from the $A C$ line through a diode bridge, and the VDD pin is charged from $\mathrm{V}_{\text {BULK }}$ through an external source-follower BiasMOS.(Figure 8-4 red path)

When the VDD pin is charged up and the voltage on the VDD pin ( $\mathrm{V}_{\text {VDD }}$ ) rises above the UVLO threshold voltage, an internal Bias circuit starts operating, and MB39C603 starts the conduction angle detection (refer to 8.3). After the UVLO is released, this device enables switching and is operating in a forced switching mode ( $\mathrm{T}_{\mathrm{ON}}=1.5 \mu \mathrm{~s}$, $\mathrm{T}_{\text {OFF }}=78 \mu \mathrm{~s}$ to $320 \mu \mathrm{~s}$ ). When the voltage on the TZE pin reaches the Zero energy threshold voltage ( $\mathrm{V}_{\text {TZETH }}=0.7 \mathrm{~V}$ ), MB39C603 enters normal operation mode. After the switching begins, the VDD pin is also charged from Auxiliary Winding through an external diode (DBIAS).(Figure 8-4 blue path)

During non-conduction period $\mathrm{V}_{\text {VDD }}$ is not supplied from $\mathrm{V}_{\text {BULK }}$ or Auxiliary Winding. It is necessary to set an appropriate capacitor of the VDD pin in order to keep $\mathrm{V}_{\text {VDD }}$ above the UVLO threshold voltage in this period. An external diode (D1) between BiasMOS and the VDD pin is used to prevent discharge from the VDD pin to $\mathrm{V}_{\text {BULK }}$ at zero cross points of the AC line voltage.

Figure 8-4 VDD Supply Path at Power-On


Figure 8-5 Power-On Waveform


MB39C603

### 8.6 Power-Off Sequence

After the AC line voltage is removed, $\mathrm{V}_{\text {BULK }}$ is discharged by switching operation and the Hold current circuit. Since any Secondary Winding current does not flow, $I_{\text {LED }}$ is supplied only from output capacitors and decreases gradually. $V_{\text {VDD }}$ also decreases because there is no current supply from both Auxiliary Winding and $\mathrm{V}_{\text {BULK }}$. When $\mathrm{V}_{\text {VDD }}$ falls below the UVLO threshold voltage, MB39C603 shuts down.

Figure 8-6 Power-Off Waveform


## 8.7 $I_{\text {P_PEAK }}$ Detection Function

MB39C603 detects Primary Winding peak current (IP_PEAK) of Transformer. I LED is set by connecting a sense resistance ( $\mathrm{R}_{\mathrm{CS}}$ ) between the CS pin and the GND pin. Maximum Ip_peak (Ip_PEAKmax) limited by Over Current Protection (OCP) can also be set with the resistance.
Using the Secondary to Primary turns ratio $\left(\mathrm{N}_{\mathrm{P}} / \mathrm{N}_{\mathrm{S}}\right)$ and ILED , $\mathrm{R}_{\mathrm{CS}}$ is set as the following equation (refer to 8.1).

$$
R_{C S}=\frac{N_{P}}{N_{S}} \times \frac{0.132}{I_{L E D}}
$$

In addition, using the OCP threshold voltage ( $\mathrm{V}_{\text {OCPTH }}$ ) and $\mathrm{R}_{\mathrm{CS}}$, IP_PEAKMAx is calculated with the following equation.

$$
I_{P_{-} P E A K M A X}=\frac{V_{O C P T H}}{R_{C S}}
$$

### 8.8 Zero Voltage Switching Function

MB39C603 has built-in zero voltage switching function to minimize switching loss of the external switching MOSFET. This device detects a zero crossing point through a resistor divider connected from the TZE pin to Auxiliary Winding. A zero energy detection circuit detects a negative crossing point of the voltage on the TZE pin to Zero energy threshold voltage ( $\mathrm{V}_{\text {TZETL }}$ ). On-timing of switching MOSFET is decided with waiting an adjustment time ( $\mathrm{t}_{\text {ADJ }}$ ) after the negative crossing occurs.
$t_{A D J}$ is set by connecting an external resistance ( $R_{A D J}$ ) between the ADJ pin and the GND pin. Using Primary Winding inductance $\left(L_{P}\right)$ and the parasitic drain capacitor of switching MOSFET ( $\mathrm{C}_{\mathrm{D}}$ ), $\mathrm{t}_{\mathrm{ADJ}}$ is calculated with the following equation.

$$
t_{A D J}=\frac{\pi \sqrt{L_{P} \times C_{D}}}{2}
$$

Using $t_{A D J}, R_{A D J}$ is set as the following equation.

$$
R_{A D J}[k \Omega]=0.0927 \times t_{A D J}[n s]
$$

### 8.9 Protection Functions

## Under Voltage Lockout Protection (UVLO)

The under voltage lockout protection (UVLO) prevents IC from a malfunction in the transient state during VVDD startup and a malfunction caused by a momentary drop of $\mathrm{V}_{\text {VDD }}$, and protects the system from destruction/deterioration. An UVLO comparator detects the voltage decrease below the UVLO threshold voltage on the VDD pin, and then the DRV pin is turned to "L" and the switching stops. MB39C603 automatically returns to normal operation mode when $\mathrm{V}_{\text {VDD }}$ increases above the UVLO threshold voltage.

## Over Voltage Protection (OVP)

The over voltage protection (OVP) protects Secondary side components from an excessive stress voltage. If the LED is disconnected, the output voltage of Secondary Winding rises up. The output overvoltage can be detected by monitoring the TZE pin. During Secondary Winding energy discharge time, $\mathrm{V}_{\text {TZE }}$ is proportional to $\mathrm{V}_{\text {Aux }}$ and the voltage of Secondary Winding (refer to 8.1). When $\mathrm{V}_{\text {TZE }}$ rises higher than the OVP threshold voltage for 3 continues switching cycles, the DRV pin is turned to "L", and the switching stops (latch off). When VvDD drops below the UVLO threshold voltage, the latch is removed.

## Over Current Protection (OCP)

The over current protection (OCP) prevents inductor or transformer from saturation. The drain current of the external switching MOSFET is limited by OCP. When the voltage on the CS pin reaches the OCP threshold voltage, the DRV pin is turned to "L" and the switching cycle ends. After zero crossing is detected on the TZE pin again, the DRV pin is turned to " H " and the next switching cycle begins.

## Over Temperature Protection (OTP)

The over temperature protection (OTP) protects IC from thermal destruction. When the junction temperature reaches $+150^{\circ} \mathrm{C}$, the DRV pin is turned to " $L$ ", and the switching stops. It automatically returns to normal operation mode if the junction temperature falls back below $+125^{\circ} \mathrm{C}$.

Table 8-2 Protection Functions Table

| Function | PIN Operation |  |  |  | Detection <br> Condition | Return <br> Condition | Remarks |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | DRV | HOLD <br> CNT | COMP | ADJ |  | - |  |
| Normal Operation | Active | Active | Active | Active | - | - |  |
| Under Voltage Lockout <br> Protection (UVLO) | L | L | L | L | $\mathrm{VDD}<8 \mathrm{~V}$ | $\mathrm{VDD}>10.2 \mathrm{~V}$ | Auto <br> Restart |
| Over Voltage <br> Protection (OVP) | L | L | 1.5 V <br> fixed | Active | $\mathrm{TZE}>4.3 \mathrm{~V}$ | VDD $<8 \mathrm{~V}$ <br> $\rightarrow \mathrm{VDD}>10.2 \mathrm{~V}$ | Latch off |
| Over Current <br> Protection (OCP) | L | Active | Active | Active | $\mathrm{CS}>2 \mathrm{~V}$ | Cycle by cycle | Auto <br> Restart |
| Over Temperature <br> Protection (OTP) | L | L | 1.5 V <br> fixed | Active | $\mathrm{Tj}>+150^{\circ} \mathrm{C}$ | $\mathrm{Tj}<+125^{\circ} \mathrm{C}$ | Auto <br> Restart |

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## 9. I/O Pin Equivalent Circuit Diagram

Figure 9-1 I/O Pin Equivalent Circuit Diagram

Pin No. | Pin |
| :---: |
| Name | TZE

Pin No. | Pin |
| :---: |
| Name | VAC

## 10. Application Examples

### 10.1 17W Isolated and Phase Dimming Application



Figure 10-1 17W EVB Schematic


MB39C603

Table 10-1 17W BOM List

| No. | Component | Description | Part No. | Vendor |
| :---: | :---: | :---: | :---: | :---: |
| 1 | M1 | LED driver IC, SOP-14 | MB39C603 | Cypress |
| 2 | Q1 | MOSFET, N-channel, 800V, 5.5A, TO-220F | FQPF8N80C | Fairchild |
| 3 | Q2 | MOSFET, N-channel, 650V, 7.3A, TO-220 | FDPF10N60NZ | Fairchild |
| 4 | Q3 | Bipolar transistor, NPN, 60V, 3A, hfe $=250 \mathrm{~min}$, SOT-223 | NZT560A | Fairchild |
| 5 | BR1 | Bridge rectifier, 1A, 600V, Micro-DIP | MDB6S | Fairchild |
| 6 | D1 | Diode, ultra fast rectifier, 1A, 600V, SMA | ES1J | Fairchild |
| 7 | D2 | Diode, ultra fast rectifier, 3A, 200V, SMC | ES3D | Fairchild |
| 8 | D3 | Diode, fast rectifier, 1A, 800V, SMA | RS1K | Fairchild |
| 9 | D4 | Diode, ultra fast rectifier, 1A, 200V, SMA | ES1D | Fairchild |
| 10 | D5 | Diode, 200 mA , 200V, SOT-23 | MMBD1404 | Fairchild |
| 11 | ZD1, ZD2 | Diode, Zener, 18V, $500 \mathrm{~mW}, \mathrm{SOD}-123$ | MMSZ18T1G | ON Semi |
| 12 | T1 | Transformer, $600 \mu \mathrm{H}$ | El-2520 | - |
| 13 | L1 | Common mode inductor, $20 \mathrm{mH}, 0.5 \mathrm{~A}$ | 744821120 | Wurth Electronic |
| 14 | L3 | Inductor, $3.3 \mathrm{mH}, 0.27 \mathrm{~A}, 5.0 \Omega$, $\phi 10 \times 14.4$ | RCH114NP-332KB | Sumida |
| 15 | C1 | Capacitor, X2, 305VAC, $0.1 \mu \mathrm{~F}$ | B32921C3104M | EPCOS |
| 16 | C2 | Capacitor, aluminum electrolytic, $100 \mu \mathrm{~F}, 25 \mathrm{~V}$, \$6.3×11 | EKMG250ELL101MF11D | NIPPON-CHEMI-CO N |
| 17 | C3 | Capacitor,polyester film, $220 \mathrm{nF}, 400 \mathrm{~V}, 18.5 \times 5.9$ | ECQ-E4224KF | Panasonic |
| 18 | C4 | Capacitor,polyester film, $100 \mathrm{nF}, 400 \mathrm{~V}, 12 \times 6.3$ | ECQ-E4104KF | Panasonic |
| 19 | C5 | Capacitor, ceramic, $10 \mu \mathrm{~F}, 50 \mathrm{~V}$, X7S, 1210 | - | - |
| 20 | C6, C7 | Capacitor, aluminum electrolytic, $470 \mu \mathrm{~F} 50 \mathrm{~V}$, \$10.0×20 | EKMG500ELL471MJ20S | $\underset{\mathrm{N}}{\text { NIPPON-CHEMI-CO }}$ |
| 21 | C8 | Capacitor, ceramic, $15 \mathrm{nF}, 250 \mathrm{~V}, \mathrm{X7R}, 1206$ | - | - |
| 22 | C9 | Capacitor, ceramic, $2.2 \mathrm{nF}, \mathrm{X} 1 / \mathrm{Y} 1$ radial | DE1E3KX222M | muRata |
| 23 | C10, C11 | Capacitor, ceramic, 0.1 FF, 50V, X5R, 0603 | - | - |
| 24 | $\begin{aligned} & \text { C12, C15, } \\ & \text { C16 } \end{aligned}$ | NA (Open), 0603 | - | - |
| 25 | C13 | Capacitor, ceramic, $10 \mu \mathrm{~F}, 35 \mathrm{~V}$, X5R, 0805 | - | - |
| 26 | C14 | Capacitor, ceramic, $4.7 \mu \mathrm{~F}, 16 \mathrm{~V}$, JB, 0805 | - | - |
| 27 | C17 | NA (Open), 1206 | - | - |
| 28 | C18 | Capacitor, ceramic, $100 \mathrm{pF}, 50 \mathrm{~V}, \mathrm{CH}, 0603$ | - | - |
| 29 | C19 | NA (Open) | - | - |
| 30 | R1, R17 | Resistor, chip, 1 M , 1/4W, 1206 | - | - |
| 31 | R2 | Resistor, metal film, 510, 2W, | - | - |
| 32 | R3 | NA (Open), 1206 | - | - |
| 33 | R4 | Resistor, metal oxide film, $68 \mathrm{k} \Omega$, 3W | - | - |
| 34 | R5 | Resistor, chip, 5.1发, 1W, 2512 | - | - |
| 35 | R6 | Resistor, chip, $62 \mathrm{k} \Omega, 1 / 10 \mathrm{~W}, 0603$ | - | - |
| 36 | R7 | Resistor, chip, 10л, 1/8W, 0805 | - | - |
| 37 | R8 | Resistor, chip, 22, 1/10W, 0603 | - | - |
| 38 | R9 | Resistor, chip, $91 \mathrm{k} \Omega, 1 / 10 \mathrm{~W}, 0603$ | - | - |
| 39 | R10 | Resistor, chip, $24 \mathrm{k} \Omega, 1 / 10 \mathrm{~W}, 0603$ | - | - |
| 40 | R11, R12 | NA (Short), 0603 | - | - |
| 41 | R13 | Resistor, chip, $39 \mathrm{k} \Omega$, 1/10W, 0603 | - | - |
| 42 | R14 | Resistor, chip, 1.1』, 1/4W, 1206 | - | - |
| 43 | R16 | Resistor, chip, $51 \mathrm{k} \Omega, 1 / 10 \mathrm{~W}, 0603$ | - | - |
| 44 | R18 | Resistor, chip, 33 k , 1/10W, 0603 | - | - |
| 45 | R19 | Resistor, chip, $12 \mathrm{k} \Omega, 1 / 10 \mathrm{~W}, 0603$ | - | - |
| 46 | R20, R15 | NA (Open), 1206 | - | - |
| 47 | R21 | Resistor, chip, 510 k , 1/10W, 0603 | - | - |
| 48 | VR1 | Varistor, 275VAC, 7 mm DISK | ERZ-V07D431 | Panasonic |
| 49 | F1 | Fuse, 1A, 300VAC | 3691100000 | Littelfuse |


| Fairchild | $:$ Fairchild Semiconductor International, Inc. |
| :--- | :--- |
| On Semi | $:$ ON Semiconductor |
| Wurth Electronic | $:$ |
| Sumida | $:$ |
| EPCOM Electronics Midcom Inc. |  |
| EPCOS | $:$ EPCOS AG |
| NIPPON-CHEMI-CON | $:$ |
| Panasonic | $:$ |
| Pappon Chemi-Con Corporation |  |
| muRata | $:$ |
| Littelfuse | $:$ |

MB39C603
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Figure 10-2 17W Reference Data

Efficiency
LED: $470 \mathrm{~mA}, 37 \mathrm{~V}$ (without Dimmer)

Power Factor
LED: $470 \mathrm{~mA}, 37 \mathrm{~V}$ (without Dimmer)


Load Regulation (without Dimmer)


MB39C603


Turn-On Waveform
$\mathrm{V}_{\mathrm{IN}}=100 \mathrm{~V}_{\mathrm{RMS}} / 60 \mathrm{~Hz}$
LED: $470 \mathrm{~mA}, 37 \mathrm{~V}$ (without Dimmer)


LED Open Waveform
$\mathrm{V}_{\mathrm{IN}}=100 \mathrm{~V}_{\text {RMS }} / 60 \mathrm{~Hz}$
LED: $470 \mathrm{~mA}, 37 \mathrm{~V}$ (without Dimmer)


Switching Waveform
$\mathrm{V}_{\text {IN }}=100 \mathrm{~V}_{\text {RMS }} / 60 \mathrm{~Hz}$
LED: 470mA, 37V (without Dimmer)


Turn-Off Waveform
$\mathrm{V}_{\text {IN }}=100 \mathrm{~V}_{\text {RMS }} / 60 \mathrm{~Hz}$


Total Harmonic Distortion(THD)
LED: $470 \mathrm{~mA}, 37 \mathrm{~V}$ (without Dimmer)


Figure 10-3 17W Japan Dimmer Performance Data


Table 10-2 17W Japan Dimmer Performance Data

| Dimmer |  | Input Condition | Type | Minimum Angle ( ${ }^{\circ}$ ) | Minimum Iout (mA) | Maximu m Angle ( ${ }^{\circ}$ ) | Maximu m Iout (mA) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Vendor | Parts Name |  |  |  |  |  |  |
| LUTRON | DVCL-123P-JA | $\begin{gathered} \mathrm{VIN}=100 \mathrm{~V}_{\text {RMS }} \\ 50 \mathrm{~Hz} \\ \text { (Japan Dimmer) } \end{gathered}$ | Leading Edge | 31.9 | 19.2 | 141.8 | 468.4 |
| Panasonic | WTC57521 |  |  | 38.0 | 19.2 | 145.6 | 467.6 |
|  | WN575280K |  |  | 27.7 | 19.8 | 147.2 | 467.0 |
|  | NQ20203T |  |  | 31.0 | 19.4 | 146.7 | 466.9 |
| DAIKO | DP-37154 |  |  | 32.4 | 19.1 | 142.9 | 466.9 |
| Mitsubishi | DEM1003B |  |  | 28.3 | 19.7 | 147.8 | 466.9 |
| TOSHIBA | DG9022H |  |  | 46.4 | 19.4 | 151.9 | 467.2 |
|  | DG9048N |  |  | 34.0 | 19.2 | 155.3 | 466.6 |
|  | WDG9001 |  | Trailing Edge | 30.4 | 18.8 | 145.4 | 468.4 |
| LUTRON | DVCL-123P-JA | $\begin{gathered} \text { VIN }=100 \mathrm{~V}_{\text {RMS }} \\ 60 \mathrm{~Hz} \\ \text { (Japan Dimmer) } \end{gathered}$ | Leading Edge | 22.7 | 19.1 | 138.5 | 468.7 |
| Panasonic | WTC57521 |  |  | 38.9 | 19.1 | 146.7 | 468.4 |
|  | WN575280K |  |  | 27.4 | 19.6 | 146.2 | 466.8 |
|  | NQ20203T |  |  | 27.6 | 19.6 | 144.3 | 467.3 |
| DAIKO | DP-37154 |  |  | 33.0 | 19.1 | 144.3 | 467.0 |
| Mitsubishi | DEM1003B |  |  | 25.9 | 19.9 | 145.2 | 467.2 |
| TOSHIBA | DG9022H |  |  | 22.0 | 18.8 | 150.8 | 467.0 |
|  | DG9048N |  |  | 22.7 | 19.6 | 153.6 | 466.5 |
|  | WDG9001 |  | Trailing Edge | 35.9 | 18.7 | 150.1 | 468.3 |

MB39C603
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Figure 10-4 17W USA Dimmer Performance Data

> Dimming Curve
> VIN $_{\text {IN }}=120 \mathrm{~V}_{\text {RMS }} / 60 \mathrm{~Hz}$
> LED: $470 \mathrm{~mA}, 37 \mathrm{~V}$


Table 10-3 17W USA Dimmer Performance Data

| Dimmer |  | Input Condition | Type | Minimum Angle ( ${ }^{\circ}$ ) | Minimum Iout (mA) | Maximu m Angle ${ }^{\circ}$ ) | Maximu m lout (mA) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Vendor | Parts Name |  |  |  |  |  |  |
| LEVITON | IPI06-1LZ | $\begin{gathered} \text { VIN }=120 \mathrm{~V}_{\text {RMS }} \\ 60 \mathrm{~Hz} \\ \text { (USA Dimmer) } \end{gathered}$ | Leading Edge | 42.3 | 25.3 | 156.0 | 477.5 |
|  | 6631-LW |  |  | 21.8 | 20.1 | 144.1 | 470.2 |
|  | 6641-W |  |  | 39.1 | 19.5 | 147.7 | 471.5 |
|  | 6683 |  |  | 35.2 | 19.5 | 155.5 | 468.9 |
| LUTRON | SLV-600-WH |  |  | 19.7 | 18.0 | 135.4 | 454.2 |
|  | S-600P-WH |  |  | 35.0 | 19.5 | 137.6 | 470.6 |
|  | TG-600PH-WH |  |  | 45.4 | 19.8 | 140.4 | 470.5 |
|  | AY-600P-WH |  |  | 40.2 | 19.5 | 143.6 | 470.6 |
|  | GL-600H-DK |  |  | 25.1 | 20.0 | 135.9 | 457.3 |
|  | TG-600PNLH-WH |  |  | 34.1 | 19.5 | 141.0 | 470.8 |
|  | TGCL-153PH-WH |  |  | 33.3 | 19.4 | 135.0 | 455.4 |
|  | TT-300NLH-WH |  |  | 41.7 | 19.5 | 143.2 | 470.5 |
|  | DV-603PG-WH |  |  | 35.6 | 19.4 | 116.4 | 316.5 |
|  | DVCL-153-WH |  |  | 38.0 | 19.4 | 133.9 | 445.7 |
|  | DV603PH-WH |  |  | 33.0 | 19.5 | 136.9 | 471.2 |
|  | LGCL-153PLH-WH |  |  | 39.3 | 19.2 | 133.9 | 444.4 |
|  | D-603PH |  |  | 24.2 | 20.0 | 133.5 | 439.1 |
|  | DV-600PH-WH |  |  | 32.8 | 19.3 | 139.3 | 470.7 |
| GE | 52129 |  |  | 23.8 | 20.2 | 157.0 | 469.8 |
|  | 18023 |  |  | 36.9 | 19.4 | 158.5 | 469.5 |
| LEVITON | IPE04-1LZ |  | Trailing Edge | 45.6 | 33.1 | 136.9 | 477.3 |
| LUTRON | SELV-300P-WH |  |  | 34.1 | 19.1 | 130.9 | 447.2 |
|  | DVELV-300P-WH |  |  | 34.1 | 19.0 | 131.8 | 455.2 |

MB39C603

Figure 10-5 17W Parts Surface Temperature


Table 10-4 17W Parts Surface Temperature Data

| Side | Cursor Point |  | Surface Temperature [ ${ }^{\circ} \mathrm{C}$ ] |  | $\Delta$ Temperature [ $\Delta^{\circ} \mathrm{C}$ ] |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 50Hz | 60 Hz | 50 Hz | 60 Hz |
| Top | a | T2 | 68.0 | 66.5 | 38.3 | 36.8 |
|  | b | Q1 | 61.8 | 61.8 | 32.2 | 32.0 |
|  | c | R4 | 70.8 | 70.1 | 41.2 | 40.3 |
|  | d | R2 | 52.8 | 52.5 | 23.1 | 22.8 |
|  | e | Q2 | 58.5 | 56.0 | 28.9 | 26.2 |
|  | f | PCB | 44.5 | 43.8 | 14.8 | 14.0 |
|  | g | Out of PCB | 29.6 | 29.8 | - | - |
| Bottom | a | M1 | 55.1 | 56.6 | 26.8 | 25.2 |
|  | b | Back side of R4 | 63.5 | 67.1 | 35.2 | 35.8 |
|  | c | BR1 | 58.0 | 61.6 | 29.7 | 30.2 |
|  | d | PCB | 45.1 | 46.9 | 16.7 | 15.5 |
|  | e | Out of PCB | 28.3 | 31.4 | - | - |

## 11. Usage Precautions

## Do not configure the IC over the maximum ratings.

If the IC is used over the maximum ratings, the LSI may be permanently damaged.
It is preferable for the device to normally operate within the recommended usage conditions. Usage outside of these conditions can have an adverse effect on the reliability of the LSI.

## Use the device within the recommended operating conditions.

The recommended values guarantee the normal LSI operation under the recommended operating conditions.
The electrical ratings are guaranteed when the device is used within the recommended operating conditions and under the conditions stated for each item.

## Take appropriate measures against static electricity.

■Containers for semiconductor materials should have anti-static protection or be made of conductive material.
■After mounting, printed circuit boards should be stored and shipped in conductive bags or containers.
■Work platforms, tools, and instruments should be properly grounded.
■Working personnel should be grounded with resistance of $250 \mathrm{k} \Omega$ to $1 \mathrm{M} \Omega$ in serial between body and ground.

## Do not apply negative voltages.

The use of negative voltages below - 0.3 V may make the parasitic transistor activated to the LSI, and can cause malfunctions.

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## 12. Ordering Information

Table 12-1 Ordering Information

| Part Number | Package | Shipping Form |
| :---: | :---: | :---: |
| MB39C603PF-G-JNEFE1 |  | Emboss |
|  |  | 14-pin plastic SOP |
| MB39C603PF-G-JNE1 | (FPT-14P-M04) |  |

## 13. Marking Format

Figure 13-1 Marking Format


MB39C603
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## 14. Recommended Mounting Condition [JEDEC Level3] Lead Free

### 14.1 Recommended Reflow Condition

Table 14-1 Recommended Reflow Condition

| Items | Contents |  |
| :---: | :---: | :---: |
| Method | IR(Infrared Reflow) $/$ Convection |  |
| Times | Before unpacking | Please use within 2 years after production. |
| Floor life | From unpacking to reflow | Within 7 days |
|  | In case over period of floor life(*1) | Baking with $125^{\circ} \mathrm{C}+/-3^{\circ} \mathrm{C}$ for $24 \mathrm{hrs}+2 \mathrm{hrs} /-$-Ohrs is required. Then <br> please use within 7 days. (Please remember baking is up to 2 <br> times) |
|  | Between $5^{\circ} \mathrm{C}$ and $30^{\circ} \mathrm{C}$ and also below $60 \%$ RH required. (It is preferred lower humidity in the required temp <br> range.) |  |

*1: Concerning the Tape \& Reel product, please transfer product to heatproof tray and so on when you perform baking. Also please prevent lead deforming and ESD damage during baking process.

### 14.2 Reflow Profile

Figure 14-1 Reflow Profile


MB39C603

## 15. Package Dimensions

| 14-pin plastic SOP | Lead pitch | 1.27 mm |
| :---: | :---: | :---: |
|  | Package width $\times$ package length | $5.3 \times 10.15 \mathrm{~mm}$ |
|  | Lead shape | Gullwing |
|  | Sealing method | Plastic mold |
|  | Mounting height | 2.25 mm MAX |
|  | Weight | 0.20 g |
| (FPT-14P-M04) | Code (Reference) | P-SOP14-5.3×10.15-1.27 |



## 16. Major Changes

Spansion Publication Number: MB39C603_DS405-00021

| Page | Section | Descriptions |
| :---: | :---: | :---: |
| Revision1.0 | - |  |
| - | Initial release |  |
| Revision2.0 |  |  |
| 7 | 7. Absolute Maximum Ratings | Removed ESD Voltage (Machine Model) from Table 7-1 |

[^0]MB39C603
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## Document History

## Document Title: MB39C603 Phase Dimmable PSR LED Driver IC for LED Lighting

## Document Number: 002-08450

| Revision | ECN | Orig. of <br> Change | Submission <br> Date | Description of Change |
| :---: | :---: | :---: | :---: | :--- |
| ${ }^{* *}$ | - | TOYO | $02 / 20 / 2015$ | Migrated to Cypress and assigned document number 002-08450. <br> No change to document contents or format. |
| ${ }^{*}$ A | 5211117 | TOYO | $04 / 07 / 2016$ | Updated to Cypress format. |

MB39C603

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[^0]:    NOTE: Please see "Document History" about later revised information.

